Solution of the first passage problem by asymptotic sampling

Christian Bucher¹ ¹ Vienna University of Technology, Vienna, Austria

1. Introduction

The first passage problem in random vibrations is readily written as a high-dimensional reliability problem. The the first passage probability or probability of failure P_F in an *n*-dimensional space of random variables $X_1, \ldots X_n$ can be computed as

$$P_F = \int \cdots \int f_{X_1,\dots,X_n}(x_1,\dots,x_n) \mathrm{d} x_1\dots \mathrm{d} x_n$$

In this equation, $f_{X_1,...,X_n}(x_1,...,x_n)$ denotes the joint probability function of the random variables $X_1,...,X_n$ and D_F denotes the failure domain, i.e. the region of the *n*-dimensional random variable space in which failure occurs. In the context of the first passage problem, this denotes combinations of input variables such that a response variable exceeds a critical threshold value. The generalized safety index (or reliability index) β is defined by

$$\beta = \Phi^{-1}(1 - P_F)$$

Here $\Phi^{-1}(.)$ is the inverse standardized Gaussian distribution function. In [2,3], a novel method called *Asymptotic sampling* is presented which avoids some of the drawbacks associated with high-dimensional reliability analysis. The underlying concept relies on the asymptotic behavior of the failure probability in *n*-dimensional i.i.d Gaussian space as the standard deviation σ of the variables and hence the failure probability P_F approaches zero (see e.g. [1]). Consider a (possibly highly nonlinear) limit state function $g(\mathbf{X})$ in which g < 0 denotes failure. Let σ be the standard deviation of the i.i.d. Gaussian variables $X_k, k = 1 \dots n$. It is attempted to determine the functional dependence of the generalized safety index β on the standard deviation σ or its inverse $f = \frac{1}{\sigma}$ by using an appropriate sampling technique. One major advantage of this approach is its independence of the dimensionality n.

2 Numerical example

This example a single-degree-of-freedom structural model with a non-linear hysteretic restoring force according to the well-known Bouc-Wen model. This structure is subject to an earthquake-type ground excitation. The excitation model used in this example is simply an amplitude-modulated white noise (shot noise). Based on this model, the earthquake excitation a(t) is generated as

$$a(t) = e(t)w(t)$$

in which w(t) is white noise with intensity D_0 , i.e. $R_{ww}(\tau) = D_0\delta(\tau)$, e(t) is a modulating function, here chosen as

$$e(t) = 4 \cdot [\exp(-0.25t) - \exp(-0.5t)]$$

In order to apply this approach in digital simulation, the continuous time white noise excitation needs to be discretized. This is achieved by representing the white noise w(t) by a sequence of i.i.d. random variables $W_k, k = 1 \dots m$ assumed to be constant values spaced at time intervals Δt . The number of random variables representing the white noise is chosen as N = 1000. The total time duration is T = 20 s, so that the time interval is $\Delta t = \frac{T}{N} = 0.02$ s. The structural model is assumed to have one kinematic degree of freedom x(t). In addition, there is an internal plastic displacement variable z(t) describing the plastic behavior of the structure. The structural model has a mass m. The equation for the derivative \dot{z} of the plastic variable depends on the state of the system. For the Bouc-Wen model this is defined by the differential equation

$$\dot{z} = A\dot{x} - \beta\dot{x}|z| - \gamma |\dot{x}|z|$$

For the state variable x we have the equations of motion:

$$m\ddot{x} + c\dot{x} + (1 - \alpha)kz + \alpha kx = -ma(t)$$

Here c is a viscous damping factor. The numerical values used in this example are k = 1 MN/m, m = 40 t, c = 5 kNs/m, $\alpha = 0.603$, $\beta = -1.8548$, $\gamma = 39.36$, A = 5.868. The equations of motion are rewritten in first-order form and then numerically. Carrying out the asymptotic sampling procedure for a displacement threshold of $\Xi = 0.5$ m yields the first passage probabilities as shown in Table 1. For reference, Monte Carlo simulation with one million samples yields the result $\beta_{MC} = 3.75$.

Table 1: Asymptotic sampling results for different number M of sample points

M	100	200	500	1000
β	3.35	3.76	3.80	3.70

References

- K. W. Breitung (1984). Asympttic approximations for multinormal integrals. *Journal of Engineering Mechanics*, 110(3):357–366.
- [2] C. Bucher (2009). Asymptotic sampling for high-dimensional reliability analysis. *Probabilistic Engineering Mechanics*, 24:504–510.
- [3] C. Bucher (2009). *Computational analysis of randomness in structural mechanics*. Structures and Infrastructures Book Series, Vol. 3. Taylor & Francis, London.