

Wave speeds in periodic elastic layers

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THE SPATIALLY periodic system of elastic layers is considered. The displacement u_i in the elementary cell consists of the displacements corresponding to the wave propagating to the left and the wave propagating to the right. The displacement u_{i+1} in the neighbouring cell is defined by u_i and the transition matrix M . It is shown that a parameter φ may be defined leading to the (essential for further calculations) relation $M(\varphi)^n = M(n\varphi)$. This relation allows us to define the phase speed. The phase speed is real for small frequencies, but for large frequencies it may be complex.

Rozpatruje się periodyczny w przestrzeni ośrodek warstwowy. Przemieszczenie u_i w komórce elementarnej jest sumą przemieszczenia odpowiadającego fali propagującej się w prawo i fali propagującej się w lewo. Przemieszczenie u_{i+1} w sąsiedniej komórce elementarnej określone jest przez u_i i macierz przejścia M . Pokazano, że można zdefiniować pewien parametr φ taki, że macierz przejścia $M = M(\varphi)$ ma istotną dla obliczeń własność $M(\varphi)^n = M(n\varphi)$. Ta własność, zupełnie taka sama jak własność liczb zespolonych, pozwala na łatwą interpretację rezultatów oraz na zdefiniowanie prędkości fazowej w układzie warstwowym. Prędkość fazowa w układzie warstwowym dla małych częstości jest rzeczywista, dla innych częstości może być zespolona.

Рассматривается периодическая в пространстве, слоистая среда. Перемещение u_i в элементарной ячейке является суммой перемещения отвечающего волне распространяющейся вправо и волны распространяющейся влево. Перемещение u_{i+1} в соседней элементарной ячейке определено через u_i и матрицу перехода M . Показано, что можно определить некоторый параметр φ , такой, что матрица перехода $M = M(\varphi)$ имеет существенное для расчетов свойство $M(\varphi)^n = M(n\varphi)$. Это свойство, вполне же такое самое как свойство комплексных чисел, позволяет легко интерпретировать результаты и определить фазовую скорость в слоистой системе. Фазовая скорость в слоистой системе для малых частот является действительной, для других частот может быть комплексной.

THE SYSTEMS of layers were dealt with in many papers, e.g. in the already classical ones [1–9]. In the present paper essential is the introduction of a new parameter φ and representation of the transition matrix $M(\varphi)$ in the form satisfying the identity $M(\varphi)^n = M(n\varphi)$. This allows us to define the phase speed in the composite.

1. Reflection and transmission

Consider the system of homogeneous elastic layers, Fig. 1. The layer situated between x_k and x_{k+1} is denoted by L_k . The Lamé constants and density of the layer L_k are denoted by $\lambda_k, \mu_k, \rho_k, k = 1, 2, 3, \dots$. In the direction x

perpendicular to the layers propagates the sinusoidal wave of frequency ω . Due to the reflections, the wave propagating in the opposite direction appears. The total displacement in the layer L_k is

$$(1.1) \quad u_k = A_k \exp i\omega [t - (x - x_k)/c_k] + B_k \exp i\omega [t + (x - x_k)/c_k],$$

where t is time, $x_k \leq x \leq x_{k+1}$, and c_k is the wave speed in the k -th layer

$$(1.2) \quad c_k^2 = (\lambda_k + 2\mu_k)/\rho_k.$$

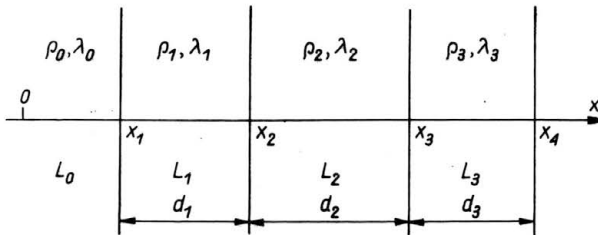


FIG. 1.

The displacement u_k consists of two parts. The first part in Eq. (1.1) represents the wave of amplitude A_k running in the x direction. The second part represents the wave of amplitude B_k running in the $-x$ direction. The displacement u_k satisfies the equation of motion

$$(1.3) \quad c_k^2 u_{k,xx} = u_{k,tt}.$$

The physical displacement is the real part of the complex-valued function $u_k(x, t)$.

At the boundary between the layers both the displacement and the stress vector are continuous. This fact leads to the relations

$$(1.4) \quad \begin{aligned} A_{k-1} \exp(-i\alpha_k) + B_{k-1} \exp(i\alpha_k) &= A_k + B_k, \\ \kappa_k [-A_{k-1} \exp(-i\alpha_k) + B_{k-1} \exp(i\alpha_k)] &= -A_k + B_k, \end{aligned}$$

where

$$(1.5) \quad \alpha_k = \omega(x_k - x_{k-1})/c_{k-1}, \quad \kappa_k = (\rho_{k-1} c_{k-1})/(\rho_k c_k).$$

Equation (1.4) may be solved for A_k, B_k to yield

$$(1.6) \quad \begin{bmatrix} A_k \\ B_k \end{bmatrix} = M_k \begin{bmatrix} A_{k-1} \\ B_{k-1} \end{bmatrix},$$

$$(1.7) \quad M_k = \frac{1}{2} \begin{bmatrix} (1 + \varkappa_k) \exp(-i\alpha_k) & (1 - \varkappa_k) \exp(i\alpha_k) \\ (1 - \varkappa_k) \exp(-i\alpha_k) & (1 + \varkappa_k) \exp(i\alpha_k) \end{bmatrix}.$$

The transition matrix M_k allows us to express A_k, B_k by A_{k-1}, B_{k-1} . The determinant of M_k depends on \varkappa_k but not on α_k ,

$$(1.8) \quad \det M_k = \varkappa_k.$$

2. Periodic layers

Consider now the case when a set of layers is repeated periodically in space. The elementary cell may consist of an arbitrary number of layers. The simplest cell consist of two layers only, Fig. 2. Denote

$$(2.1) \quad \varkappa = (\rho_a c_a)/(\rho_b c_b), \quad \alpha_a = \omega d_a/c_a, \quad \alpha_b = \omega d_b/c_b;$$

$$(2.2) \quad M_a = \frac{1}{2} \begin{bmatrix} (1 + \varkappa) \exp(-i\alpha_a) & (1 - \varkappa) \exp(i\alpha_a) \\ (1 - \varkappa) \exp(-i\alpha_a) & (1 + \varkappa) \exp(i\alpha_a) \end{bmatrix},$$

$$M_b = \frac{1}{2} \begin{bmatrix} (1 + 1/\varkappa) \exp(-i\alpha_b) & (1 - 1/\varkappa) \exp(i\alpha_b) \\ (1 - 1/\varkappa) \exp(-i\alpha_b) & (1 + 1/\varkappa) \exp(i\alpha_b) \end{bmatrix}.$$

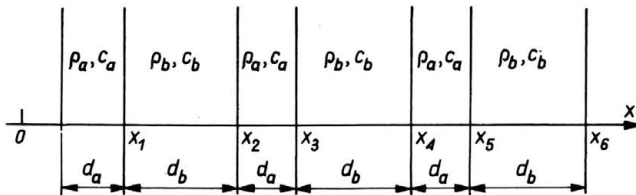


FIG. 2.

Therefore

$$\begin{array}{llll} \varkappa_k = \varkappa, & c_k = c_a, & \alpha_k = \alpha_a, & M_k = M_a \quad \text{for } k = 0, 2, 4, \dots, \\ \varkappa_k = 1/\varkappa & c_k = c_b, & \alpha_k = \alpha_b, & M_k = M_b \quad \text{for } k = 1, 3, 5, \dots \end{array}$$

In the above formulae M_a is the transition matrix from a to b , and M_b the transition matrix from b to a .

The purpose of the further analysis is to calculate the average wave speed in the set of layers. Concentrate first on the displacements in the layers of type a . In accord with Eq. (1.6), for each integer n there is

$$(2.3) \quad \begin{bmatrix} A_{2n} \\ B_{2n} \end{bmatrix} = M^n \begin{bmatrix} A_0 \\ B_0 \end{bmatrix}, \quad M = M_b M_a, \quad n = 1, 2, 3, \dots,$$

where M is the transition matrix for one cell. From Eq. (2.2) it follows that this transition matrix has the following components:

$$(2.4) \quad \begin{aligned} 4 M_{11} &= (2 + \kappa + 1/\kappa) \exp i(-\alpha_a - \alpha_b) + (2 - \kappa - 1/\kappa) \exp i(-\alpha_a + \alpha_b), \\ 4 M_{21} &= (\kappa - 1/\kappa) \exp i(-\alpha_a - \alpha_b) - (\kappa + 1/\kappa) \exp i(-\alpha_a + \alpha_b), \end{aligned}$$

$$(2.5) \quad M_{22} = \overline{M_{11}}, \quad M_{12} = \overline{M_{21}}.$$

Note that the matrix M is non-Hermitian since M_{11} is not real. The matrix with the symmetry (2.5) will be further called W -symmetric. The product of two W -symmetric matrices is W -symmetric. The matrix M is the periodic function of α_a and α_b .

For $\kappa = 2$, $d_a = 2d_b$ some displacement profiles are given in Figs. 3–6. For $\alpha_a = \alpha_b = 0.1$ (Fig. 3), $\alpha_a = \alpha_b = 0.5$ (Fig. 4) and $\alpha_a = \alpha_b = 1$ (Fig. 5), the

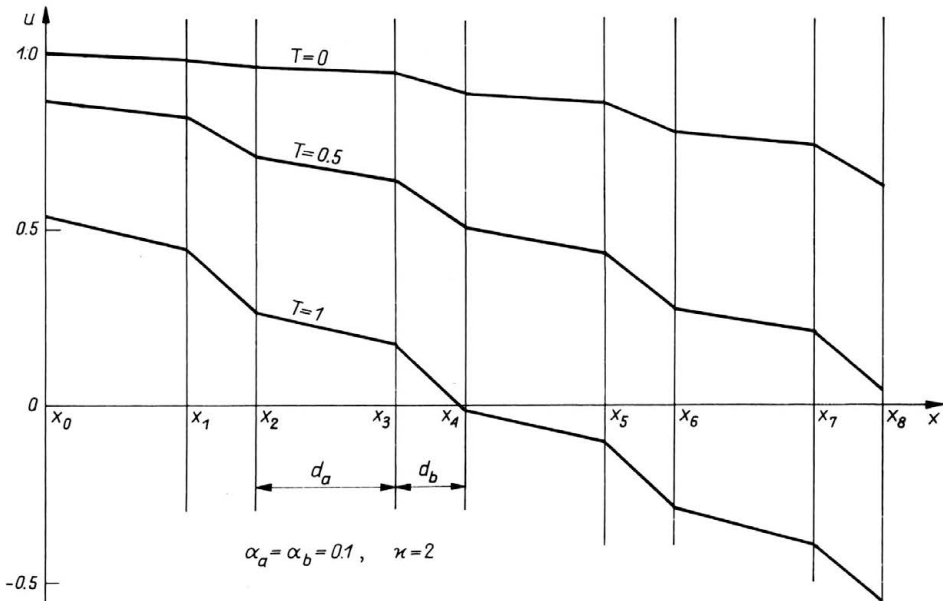


FIG. 3.

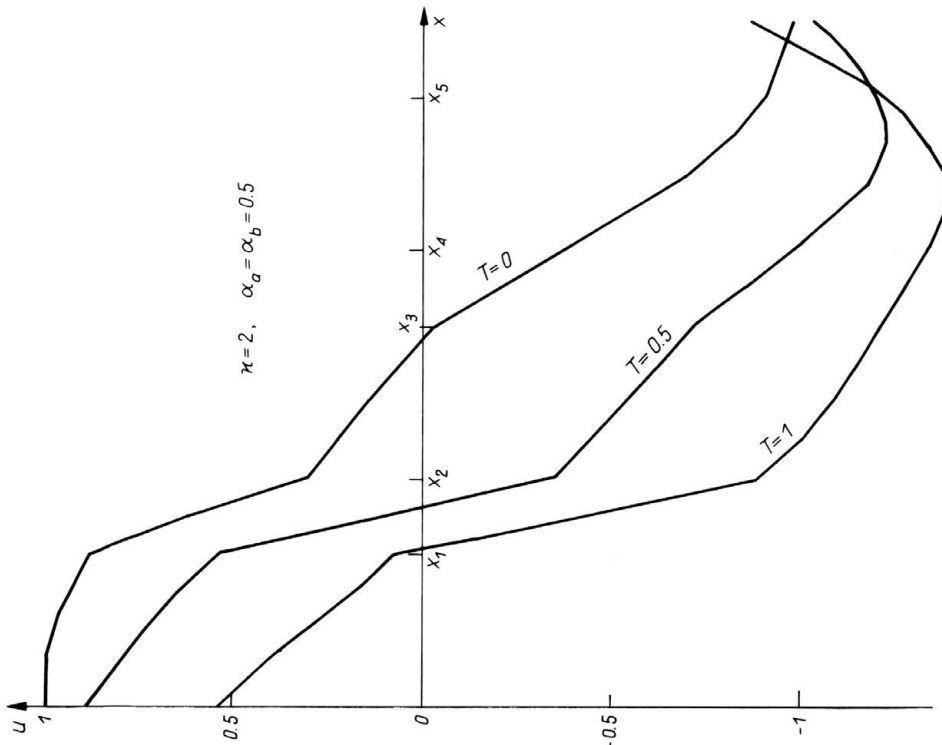


FIG. 4.

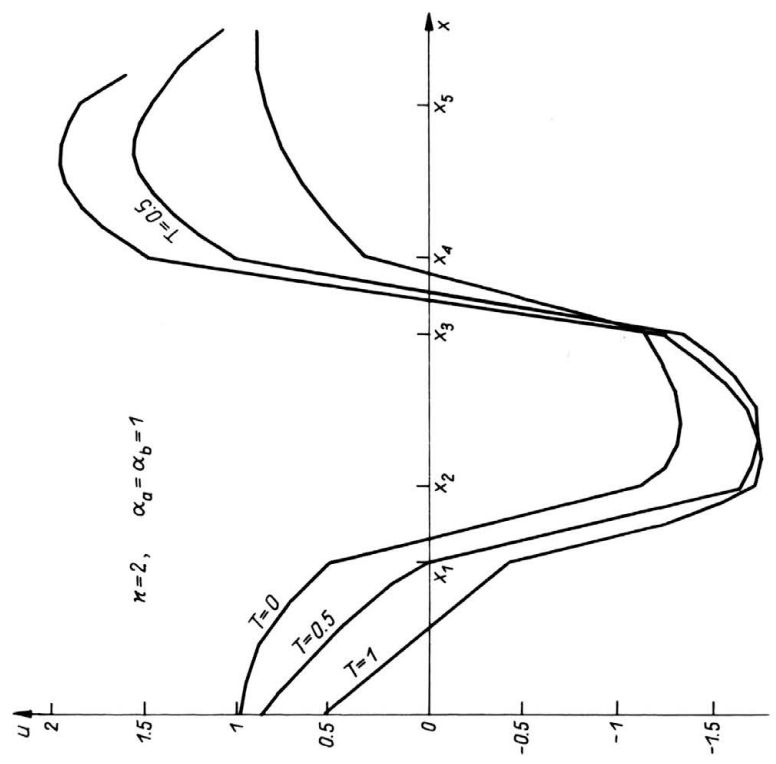


FIG. 5.

displacement remains small in each cell. For $\alpha_a = \alpha_b = 1.4$ (Fig. 6) the displacement grows exponentially with n .

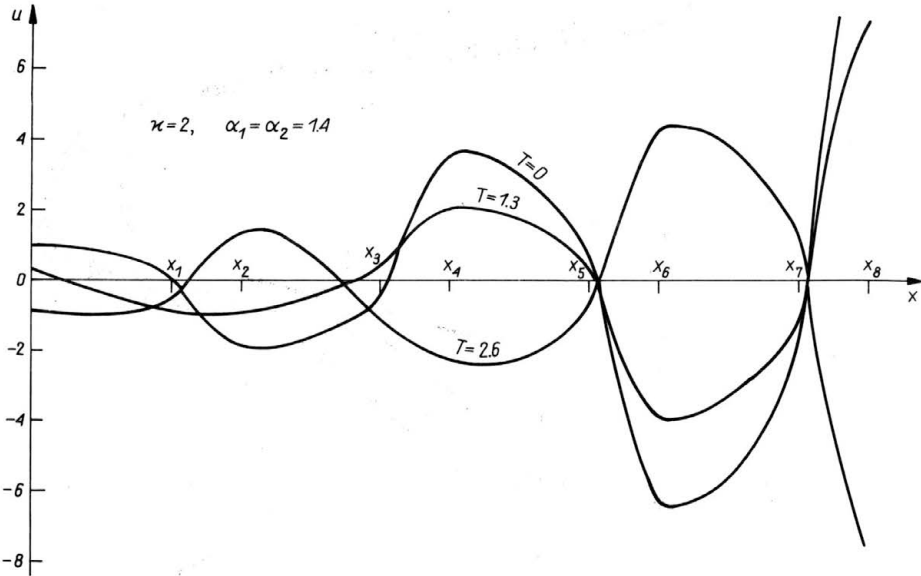


FIG. 6.

Consider first the case when ω is sufficiently small. Then $\text{Re } M_{11} < 1$ and, in accord with the derivation given in the Appendix, the matrix M may be written in the form

$$(2.6) \quad M = \begin{bmatrix} \cos \varphi - iE \sin \varphi & (C + iD) \sin \varphi \\ (C - iD) \sin \varphi & \cos \varphi + iE \sin \varphi \end{bmatrix},$$

$$(2.7) \quad \varphi = \arccos H, \quad H = \text{Re } M_{11},$$

$$(2.8) \quad E^2 - C^2 - D^2 = 1,$$

where φ , E , C , D are real parameters. The important identity holds

$$(2.9) \quad M^n = \begin{bmatrix} \cos n\varphi - iE \sin n\varphi & (C + iD) \sin n\varphi \\ (C - iD) \sin n\varphi & \cos n\varphi + iE \sin n\varphi \end{bmatrix}, \quad n = 1, 2, \dots$$

Figure 7 shows, for fixed κ , the values of α_a , α_b for which $-1 < H < 1$ and φ is real. For fixed κ the region between the curves corresponds to $H < -1$.

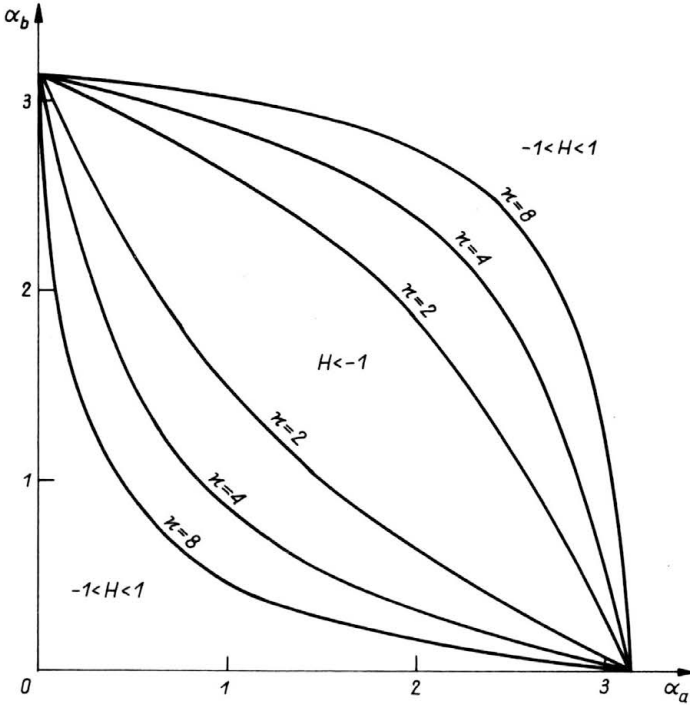


FIG. 7.

The smaller is κ , the larger is the region for which φ is real. Because of the periodicity of M , the picture repeats for larger values of α_a, α_b . For $\kappa = 2$ the regions are shown in Fig. 8.

Calculate the displacement at the beginning of each layer of the kind a , therefore at the discrete set of points

$$(2.10) \quad x_n = n(d_a + d_b), \quad n = 1, 2, 3, \dots$$

In accord with Eqs. (1.1), (2.3) and (2.9), we obtain

$$(2.11) \quad u(x_n, t) = \{ [M_{11}(n\varphi) + M_{21}(n\varphi)] A_0 + [M_{12}(n\varphi) + M_{22}(n\varphi)] B_0 \} \exp i\omega t$$

or, in terms of the parameters φ, C, D, E ,

$$(2.12) \quad u(x_n, t) = \{ [\cos n\varphi + (C - iE - iD) \sin n\varphi] A_0 + [\cos n\varphi + (C + iE + iD) \sin n\varphi] B_0 \} \exp i\omega t.$$

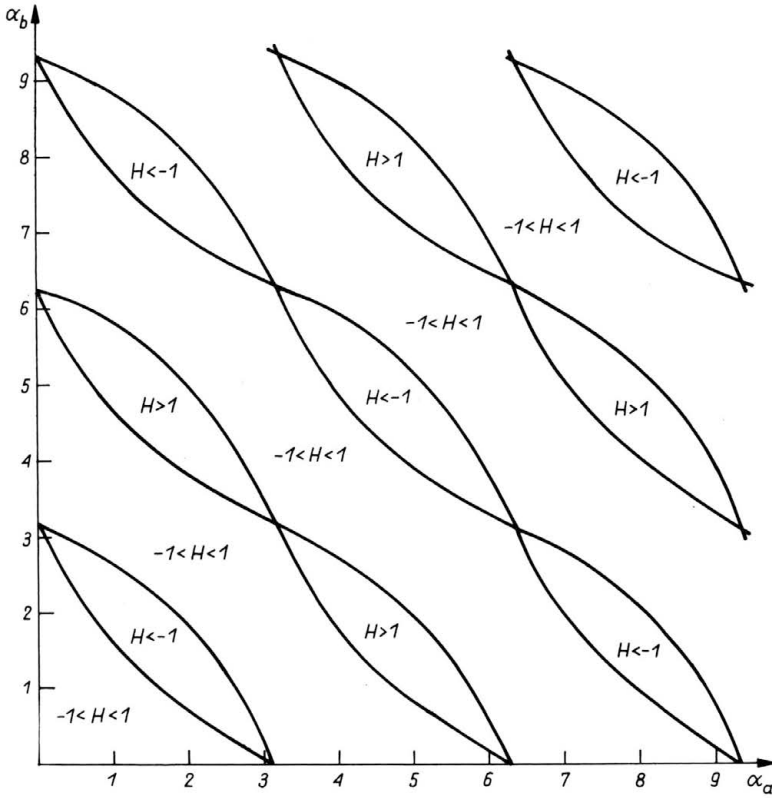


FIG. 8.

The physical displacement is the real part of u as given by the Eq. (2.12)

$$(2.13) \quad \text{Re}(u) = (A_0 + B_0)(\cos n\varphi + C \sin n\varphi) \cos \omega t + (A_0 - B_0)(E + D) \sin n\varphi \sin \omega t.$$

Simple trigonometric transformations lead to the formula

$$(2.14) \quad \begin{aligned} \text{Re}(u) &= w_R + w_L, \\ 2w_R &= A_0 [(1 + E + D) \cos(\omega t - n\varphi) - C \sin(\omega t - n\varphi)] \\ &\quad + B_0 [(1 - E - D) \cos(\omega t - n\varphi) - C \sin(\omega t - n\varphi)], \\ 2w_L &= A_0 [(1 - E - D) \cos(\omega t + n\varphi) + C \sin(\omega t + n\varphi)] \\ &\quad + B_0 [(1 + E + D) \cos(\omega t + n\varphi) + C \sin(\omega t + n\varphi)]. \end{aligned}$$

The waves with the phase $(\omega t - n\varphi)$ run to the right, and the waves with the phase $(\omega t + n\varphi)$ run to the left. Note that the amplitudes of all waves are constant and do not depend on n , in contrast to the amplitudes A_k, B_k

in Eq. (2.3) which are functions of n . The arguments of the trigonometric functions (phase) do depend on n . Using Eq. (2.10) we obtain the formulae for phases f_R and f_L of the waves running to the right and the left

$$(2.15) \quad f_R = \omega t - \varphi x_n (d_a + d_b)^{-1}, \quad f_L = \omega t + \varphi x_n (d_a + d_b)^{-1},$$

or, in accord with Eq. (2.1), the formulae

$$(2.16) \quad \begin{aligned} f_R &= \omega [t - \varphi x_n (\alpha_a c_a + \alpha_b c_b)^{-1}], \\ f_L &= \omega [t + \varphi x_n (\alpha_a c_a + \alpha_b c_b)^{-1}]. \end{aligned}$$

Both formulae hold for the discrete set of points $x = n(d_a + d_b)$ and arbitrary t . It follows that the phase speed c of the waves w_R and w_L is given by the formula

$$(2.17) \quad c = (\alpha_a c_a + \alpha_b c_b) / \varphi,$$

or, using Eq. (2.8), in the explicit form

$$(2.18) \quad c = (\alpha_a c_a + \alpha_b c_b) / \arccos(\operatorname{Re} M_{11}).$$

It is seen from Eq. (2.4) that $\varphi = \varphi(\omega)$. Therefore, in accord with the above formula, we obtain $c = c(\omega)$ and the system of layers is dispersive. By differentiation of c with respect to ω the group speed $c_g = dc/d\omega$ may be obtained. Note that for the homogeneous system $\kappa = 1$ and

$$(2.19) \quad \operatorname{Re} M_{11} = \cos(\alpha_a + \alpha_b), \quad \varphi = \alpha_a + \alpha_b, \quad c = \frac{\alpha_a c_a + \alpha_b c_b}{\alpha_a + \alpha_b}.$$

In this case the speed c does not depend on ω and the system is non-dispersive. The curves $c(\omega)$ for some speed ratios will be shown in the next Section.

In the above calculations only the points $x = x_{2k}$ were taken into account. The question arises what speed is obtained for other points. We shall show that Eq. (2.18) holds for other points too. Take $x = x_{2k} + p$, where p is fixed, $0 < p < d_a$, and consider the periodic system consisting of three layers, Fig. 9. The three layers are introduced purely formally. Physically this system does not differ from the two-layered system considered above. The layers of thickness p and $d_a - p$ are of the material a and the layer of thickness d_b of the material b . Denoting

$$(2.20) \quad \gamma = \omega \frac{P}{c_a},$$

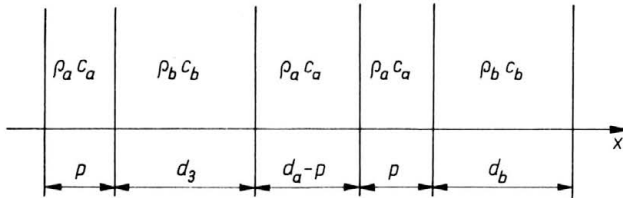


FIG. 9.

we obtain the transition matrix M^* in the form of a product of three matrices

$$(2.21) \quad M^* = \begin{bmatrix} \exp i(-\alpha_a + \gamma) & 0 \\ 0 & \exp i(\alpha_a + \gamma) \end{bmatrix} \cdot \begin{bmatrix} (1 + 1/\kappa) \exp(-i\alpha_b) & (1 - 1/\kappa) \exp(i\alpha_b) \\ (1 - 1/\kappa) \exp(-i\alpha_b) & (1 + 1/\kappa) \exp(i\alpha_b) \end{bmatrix} \cdot \begin{bmatrix} (1 + \kappa) \exp(-i\gamma) & (1 - \kappa) \exp(i\gamma) \\ (1 - \kappa) \exp(-i\gamma) & (1 + \kappa) \exp(i\gamma) \end{bmatrix}.$$

After calculating the product we obtain $M_{11}^* = M_{11}$ what leads to

$$(2.22) \quad \varphi^* = \varphi.$$

It follows that the phase speed c^* equals c for each point situated in the layer a . On the other hand, $\text{Re } M_{11}$ as given by Eq (2.4), is invariant with respect to the interchange $a \rightarrow b$. Summarizing: the phase speed c is the same for each point of the elementary cell.

Above we have assumed $-1 < \text{Re } M_{11} < 1$. If these inequalities do not hold, we face other cases described in the Appendix. Then in the formula (2.12), instead of the trigonometric functions $\cos \varphi$, $\sin \varphi$, the hyperbolic functions $\text{ch } \varphi$, $\text{sh } \varphi$ appear. This leads to the exponential growth or exponential decay of the displacements. In this case the phase speed c is complex-valued. The frequency ω_1 for which $\text{Re } M_{11} = 1$ or -1 will be called critical. For small ω the speed c is always real.

3. Average speeds

Before analyzing the formula (2.18) for the phase speed, let us define two other speeds. The wave travelling with speed c_a in the layer L_a and speed c_b in the layer L_b covers the distance $d_a + d_b$ in the time interval $d_a/c_a + d_b/c_b$. The first average speed c_1 is defined by the relation

$$(3.1) \quad (d_a + d_b)/c_1 = d_a/c_a + d_b/c_b.$$

From Eq. (2.1) it follows

$$(3.2) \quad c_1 = (\alpha_a c_a + \alpha_b c_b)/(\alpha_a + \alpha_b).$$

Define next the second average speed c_2 . Denote by ρ and E the density and Young modulus of the hypothetic homogeneous material possessing the same mass and rigidity as the system of layers. Due to a tensile stress σ in the x -direction, the unit cell and the homogeneous material have the same elongation. Therefore ρ and E are defined by the relations (cf. Fig. 10)

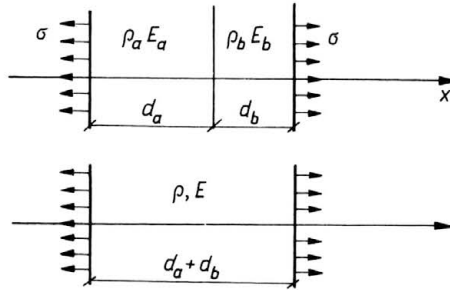


FIG. 10.

$$(3.3) \quad \begin{aligned} \rho(d_a + d_b) &= \rho_a d_a + \rho_b d_b, \\ (d_a + d_b)\sigma/E &= d_a \sigma/E_a + d_b \sigma/E_b, \end{aligned}$$

which lead to

$$(3.4) \quad \rho = (\rho_a d_a + \rho_b d_b)/(d_a + d_b),$$

$$(3.5) \quad E = (d_a + d_b)/(d_a/E_a + d_b/E_b).$$

In the homogeneous material the Young modulus is the product of the density and the squared propagation speed. Define the squared speed c_2 as the ratio E/ρ . Then

$$(3.6) \quad c_2^2 = \frac{(d_a + d_b)^2}{(d_a/E_a + d_b/E_b)(\rho_a d_a + \rho_b d_b)}.$$

Basing on Eq. (2.1) this formula may be transformed to the two equivalent formulae

$$(3.7) \quad c_2^2 = \frac{(\alpha_a c_a + \alpha_b c_b)^2}{\alpha_a^2 + \alpha_b^2 + (\kappa + 1/\kappa)\alpha_a \alpha_b},$$

$$(3.8) \quad c_2^2 = c_1^2 \frac{(\alpha_a + \alpha_b)^2}{\alpha_a^2 + \alpha_b^2 + (\kappa + 1/\kappa) \alpha_a \alpha_b}.$$

Since for each κ we have $(\kappa + 1/\kappa) \geq 2$, it follows from Eq. (3.8) that $c_2 \leq c_1$.

Analyse now the formula (2.17) for the phase speed c . Calculate first the speed c for small α_a, α_b , i.e. for small frequency ω . In accord with Eq. (2.4) we have

$$(3.9) \quad \begin{aligned} M_{11} = & [(2 + \kappa + 1/\kappa) \cos \omega (d_a/c_a + d_b/c_b) \\ & + (2 - \kappa - 1/\kappa) \cos \omega (d_a/c_a - d_b/c_b)]/4 \\ \approx & 1 - \frac{\omega^2}{2} \left[\left(\frac{d_a}{c_a}\right)^2 + \left(\frac{d_b}{c_b}\right)^2 + \left(\kappa + \frac{1}{\kappa}\right) \frac{d_a d_b}{c_a c_b} \right], \\ \varphi \approx & \left[\alpha_a^2 + \alpha_b^2 + \left(\kappa + \frac{1}{\kappa}\right) \alpha_a \alpha_b \right]^{1/2}. \end{aligned}$$

Substitution of the last result into Eq. (2.17) yields the approximate relation

$$(3.10) \quad c \approx (\alpha_a c_a + \alpha_b c_b) \left[\alpha_a^2 + \alpha_b^2 + \left(\kappa + \frac{1}{\kappa}\right) \alpha_a \alpha_b \right]^{-1/2}.$$

Comparison with Eq. (3.7) leads to the conclusion that for $\omega \Rightarrow 0$ also $c \Rightarrow 0$. In view of the periodicity of M , the same result holds for other ω , provided $\alpha_a \Rightarrow 2\pi n_1, \alpha_b \Rightarrow 2\pi n_2$, where n_1, n_2 are integers.

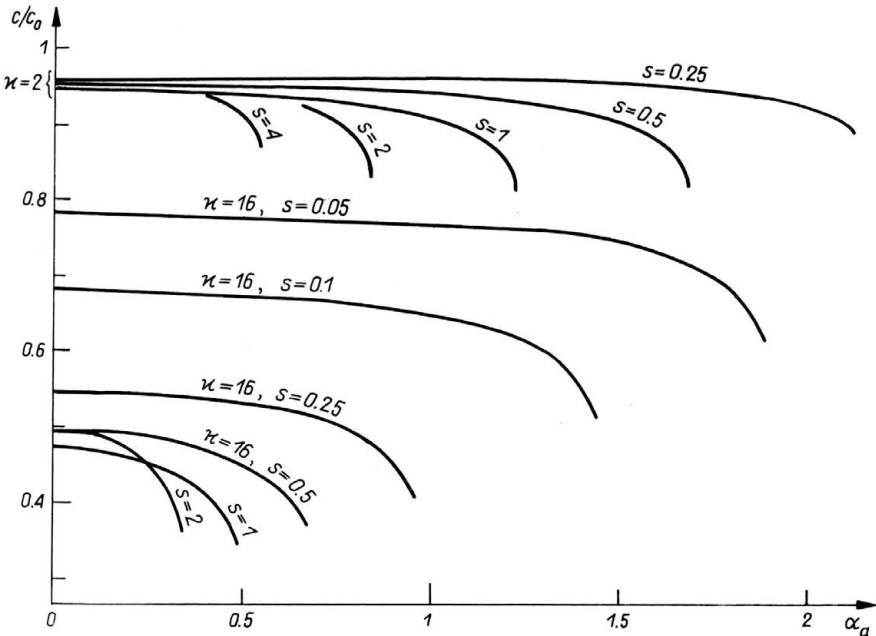


FIG. 11.

Figure 11 gives the functions c/c_0 for $\kappa = 2$ and $\kappa = 16$ for several ratios $s = \alpha_b/\alpha_a$. For each s , ratio c/c_0 is a decreasing function of ω . At $\alpha_a = 0$ there is $c = c_2$. The function being monotonically decreasing for each frequency ω we have

$$(3.11) \quad c \leq c_2.$$

Due to the periodicity it was assumed that $\varphi \leq 2\pi$.

The above analysis concerned the case when the elementary cell consisted of two layers only. It is straightforward to generalize the results to any number N of layers in the primitive cell. The transition matrices for the layers are then

$$(3.12) \quad M_{a_k} = \frac{1}{2} \begin{bmatrix} (1 + \kappa_{a_k}) \exp(-i\alpha_{a_k}) & (1 - \kappa_{a_k}) \exp(i\alpha_{a_k}) \\ (1 - \kappa_{a_k}) \exp(-i\alpha_{a_k}) & (1 + \kappa_{a_k}) \exp(i\alpha_{a_k}) \end{bmatrix},$$

$$(3.13) \quad \det M_{a_k} = \kappa_{a_k}, \quad k = 1, 2, 3, \dots, N - 1,$$

$$(3.14) \quad M_{a_N} = \frac{1}{2} \begin{bmatrix} (1 + \xi) \exp(-i\alpha_{a_N}) & (1 - \xi) \exp(i\alpha_{a_N}) \\ (1 - \xi) \exp(-i\alpha_{a_N}) & (1 + \xi) \exp(i\alpha_{a_N}) \end{bmatrix},$$

$$(3.15) \quad \begin{aligned} \xi &= 1/(\kappa_{a_1} \kappa_{a_2} \dots \kappa_{a_{N-1}}), \\ \det M_{a_N} &= 1/(\kappa_{a_1} \kappa_{a_2} \dots \kappa_{a_{N-1}}). \end{aligned}$$

The transition matrix (3.14) has a special form because it describes the transition back to the first material. Note that each of the above matrices is W -symmetric, therefore their product is W -symmetric. Moreover, their determinant equals 1 due to Eqs. (3.15). It follows that the product of the N matrices (3.12), (3.14) satisfies Eq. (2.5), therefore the parameter φ may be introduced. The qualitative results obtained for two layers in the primitive cell hold for arbitrary number of layers in this cell.

Appendix

Consider the 2×2 complex-valued matrix M satisfying the relations

$$(A.1) \quad M_{21} = \overline{M_{12}}, \quad M_{22} = \overline{M_{11}},$$

$$(A.2) \quad \det M = 1.$$

The matrix with symmetry (A.1) will be called W -symmetric. The product of two W -symmetric matrices is W -symmetric. In general, the W -symmetric matrix is non-Hermitean.

Three cases are possible: either $-1 < \operatorname{Re} M_{11} < 1$, or $\operatorname{Re} M_{11} \geq 1$, or $\operatorname{Re} M_{11} \leq -1$. Consider first

$$(A.3) \quad -1 < \operatorname{Re} M_{11} < 1.$$

Without losing the generality assume the range $0 < \varphi < \pi$ and write the matrix M in the following form:

$$(A.4) \quad M = \begin{bmatrix} \cos \varphi - iE \sin \varphi & (C + iD) \sin \varphi \\ (C - iD) \sin \varphi & \cos \varphi + iE \sin \varphi \end{bmatrix},$$

where the real parameters φ, E, C, D are uniquely determined by the relations

$$(A.5) \quad \varphi = \arccos(\operatorname{Re} M_{11}),$$

$$(A.6) \quad E \sin \varphi = \operatorname{Im} M_{22}, \quad C \sin \varphi = \operatorname{Re} M_{12}, \quad D \sin \varphi = \operatorname{Im} M_{12}.$$

The relation (A.2) leads to

$$(A.7) \quad E^2 - C^2 - D^2 = 1.$$

By mathematical induction we prove now the formula

$$(A.8) \quad M^n = \begin{bmatrix} \cos n\varphi - iE \sin n\varphi & (C + iD) \sin n\varphi \\ (C - iD) \sin n\varphi & \cos n\varphi + iE \sin n\varphi \end{bmatrix}.$$

Multiplying by M we get

$$(A.9) \quad \begin{aligned} M_{11}^{n+1} &= \cos n\varphi \cos \varphi - (E^2 - C^2 - D^2) \sin n\varphi \sin \varphi - iE \sin(n+1)\varphi, \\ M_{21}^{n+1} &= (C - iD) \sin(n+1)\varphi, \quad M_{22}^{n+1} = \overline{M_{11}^{n+1}}, \quad M_{12}^{n+1} = \overline{M_{21}^{n+1}}. \end{aligned}$$

Taking now into account Eqs. (A.7), we obtain

$$(A.10) \quad M^{n+1} = \begin{bmatrix} \cos(n+1)\varphi - iE \sin(n+1)\varphi & (C + iD) \sin(n+1)\varphi \\ (C - iD) \sin(n+1)\varphi & \cos(n+1)\varphi + iE \sin(n+1)\varphi \end{bmatrix},$$

what is exactly the formula (A.8) for the power $(n+1)$. The fact that (A.8) holds for $n=1$ completes the proof.

In the cases $\operatorname{Re} M_{11} > 1$ and $\operatorname{Re} M_{11} < -1$ the above results may be used provided we allow for complex-valued φ . In the practical calculations, however, it is more convenient to introduce the hyperbolic functions and real parameter ψ , and to re-define the other constants.

Consider first

$$(A.11) \quad \operatorname{Re} M_{11} > 1.$$

Defining

$$(A.12) \quad \psi = \operatorname{Arch}(\operatorname{Re} M_{11}),$$

we can represent M in the form

$$(A.13) \quad M = \begin{bmatrix} \operatorname{ch}\psi - iE \operatorname{sh}\psi & (C + iD) \operatorname{sh}\psi \\ (C - iD) \operatorname{sh}\psi & \operatorname{ch}\psi + iE \operatorname{sh}\psi \end{bmatrix},$$

where the constants E, C, D (other than in the trigonometric case) are defined by the relations

$$(A.14) \quad E \operatorname{sh}\psi = \operatorname{Im} M_{22}, \quad C \operatorname{sh}\psi = \operatorname{Re} M_{12}, \quad D \operatorname{sh}\psi = \operatorname{Im} M_{12}.$$

The condition $\det M = 1$ leads to

$$(A.15) \quad -E^2 + C^2 + D^2 = 1.$$

By the mathematical induction, exactly in the same manner as in the trigonometric case, it may be shown that

$$(A.16) \quad M^n = \begin{bmatrix} \operatorname{chn}\psi - iE \operatorname{shn}\psi & (C + iD) \operatorname{shn}\psi \\ (C - iD) \operatorname{shn}\psi & \operatorname{chn}\psi + iE \operatorname{shn}\psi \end{bmatrix}.$$

For

$$(A.17) \quad \operatorname{Re} M_{11} < -1,$$

$$(A.18) \quad \psi = \operatorname{Arch}(-M_{11}),$$

we have the following form of the matrix M :

$$(A.19) \quad M = \begin{bmatrix} \operatorname{ch}\psi - iE \operatorname{sh}\psi & (C + iD) \operatorname{sh}\psi \\ (C - iD) \operatorname{sh}\psi & \operatorname{ch}\psi + iE \operatorname{sh}\psi \end{bmatrix},$$

where the real parameters E, C, D are uniquely defined by the relations

$$(A.20) \quad -E \operatorname{sh}\psi = \operatorname{Im} M_{22}, \quad -C \operatorname{sh}\psi = \operatorname{Re} M_{12}, \quad -D \operatorname{sh}\psi = \operatorname{Im} M_{12}.$$

From $\det M = 1$ it follows that

$$(A.21) \quad -E^2 + C^2 + D^2 = 1,$$

$$(A.22) \quad M = (-1)^n \begin{bmatrix} \operatorname{chn}\psi - iE \operatorname{shn}\psi & (C + iD) \operatorname{shn}\psi \\ (C - iD) \operatorname{shn}\psi & \operatorname{chn}\psi + iE \operatorname{shn}\psi \end{bmatrix}.$$

The cases $\operatorname{Re} M_{11} = 1$ and $\operatorname{Re} M_{11} < -1$ are not included in the formula (A.3) because then E tends to infinity. Elementary calculations show that for $\operatorname{Re} M_{11} = 1$ we obtain

$$(A.23) \quad M = \begin{bmatrix} 1 - iE & C + iD \\ C - iD & 1 + iE \end{bmatrix}, \quad M^n = \begin{bmatrix} 1 - inE & n(C + D) \\ n(C - iD) & 1 + inE \end{bmatrix},$$

and for $\operatorname{Re} M_{11} = -1$

$$(A.24) \quad M = - \begin{bmatrix} 1 - iE & C + iD \\ C - iD & 1 + iE \end{bmatrix}, \quad M^n = (-1)^n \begin{bmatrix} 1 - inE & n(C + D) \\ n(C - iD) & 1 + inE \end{bmatrix}.$$

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